



SUMMER-18 EXAMINATION
Model Answer

Subject Title: Mass Transfer Operation

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Important Instructions to examiners:

- 1) The answers should be examined by key words and not as word-to-word as given in the model answer scheme.
- 2) The model answer and the answer written by candidate may vary but the examiner may try to assess the understanding level of the candidate.
- 3) The language errors such as grammatical, spelling errors should not be given more Importance (Not applicable for subject English and Communication Skills).
- 4) While assessing figures, examiner may give credit for principal components indicated in the figure. The figures drawn by candidate and model answer may vary. The examiner may give credit for any equivalent figure drawn.
- 5) Credits may be given step wise for numerical problems. In some cases, the assumed constant values may vary and there may be some difference in the candidate's answers and model answer.
- 6) In case of some questions credit may be given by judgement on part of examiner of relevant answer based on candidate's understanding.
- 7) For programming language papers, credit may be given to any other program based on equivalent concept.



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Q No.	Answer	Marking scheme
1 a	Attempt any 3	12
1A-a	Different terms involved in two film theory: K_y – Overall mass transfer coefficient $m = \text{slope} = (y_{Ai} - y_A^*) / (x_{Ai} - x_A)$ y_{Ai} - concentration of solute at vapour interface y_A^* - composition of solute in gas phase which is in equilibrium with x_A x_{Ai} - concentration of solute at the liquid interface x_A – concentration of solute in bulk liquid k_y – mass transfer coefficient in vapour phase k_x - mass transfer coefficient in liquid phase	4
1A-b	Raoult's law: It states that at a given temperature, the partial pressure of a component A is equal to the product of mol fraction of the component A in the liquid phase and the vapour pressure of the pure component A $p_A = p_A^0 x_A$ where, p_A - partial pressure of A p_A^0 - vapour pressure of the pure component A x_A - mol fraction of the component A in liquid phase i) Daltons law : It states that the total pressure exerted by gas/vapour mixture is equal to the sum of the partial pressures of components present in it, thus it expresses the additive nature of the partial pressure. Mathematically, for binary system $P = p_A + p_B$	1 1 1 1



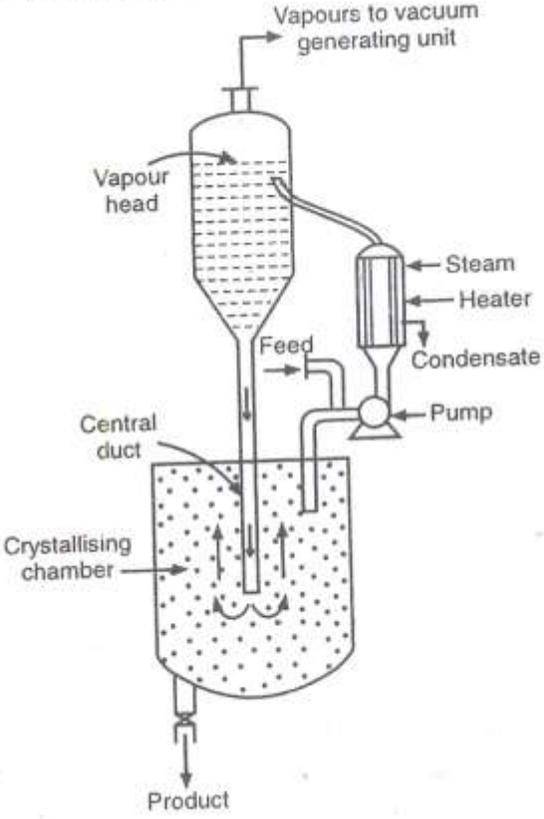
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	<p>2. Providing good liquid distribution system.</p> <p>Channeling leads to flooding and loading: When channeling occurs, liquid flows along the walls and liquid hold up in the column starts to increase. This is loading. When the gas velocity increases further, entrainment of liquid by the gas leaving the top of the tower increases and flooding of tower takes place.</p>	2
1B-b	<p>Oslo evaporative crystallizer:</p>  <p>In this crystallizer, super saturation is generated or achieved by evaporation.</p> <p>Construction:</p> <p>It consist of a crystallizing chamber containing a bed of forming and growing crystals .A circulating pump and external heater for heating the solution with the help of condensing steam and a vapor head maintained by a vacuum</p>	2



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	<p>generating equipment.</p> <p>Working: The solution from crystallizing chamber is pump by a circulating pump on the suction side of which the feed solution forming a small part of the total circulating liquid is introduced into a heater. Where it is heated by means of condensing steam and then fed to a vap head where some of the solution flashes into vap resulting into some degree of super saturation. The supersaturated solution is returned to the bottom of the crystallizing chamber through a central duct into a crystallizing chamber.</p> <p>Nucleation takes place in the crystal blade which is maintained In a fluidized state by means of upward flowing steam. Then the nuclei converted to crystal of required size and withdrawn as product from the bottom.</p>	2
2	Attempt any 4	16
2-a	<p>Factors on which the rate of drying depends:</p> <ol style="list-style-type: none">1) Gas Velocity: When the velocity of the gas or air is high the rate of drying will also be high.2) Humidity of gas : Lesser the relative humidity, the more will be the rate of drying.3) Area of drying surface: If the area of the wet surface exposed to the gas or air is more, the rate of drying will also be more.4) Temperature: If the temperature of the gas is increased' it's relative humidity decreases (i.e gas becomes more unsaturated) and thus increase a driving force (i.e the concentration difference of moisture between the solid and gas) and so the rate of drying increases.	1 mark each
2-b	<p>Working of fluidized bed dryer: A fluidized bed system in addition to a fluidizing chamber also needs an air blower, a hot air generator, a feed conveyor, a cyclone separator and a product conveyor.</p> <p>In this drier, hot air is used to keep the wet feed in a fluidized state. In the drier</p>	4



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	<p>the wet material is dried and cooled in the same bed. Wet feed material is admitted to the top of the bed through a hopper via a rotary valve and hot air is distributed at the bottom of the bed through a diffuser plate and dry product is taken out from the side or near the bottom. Heat and mass transfer coefficient are high because of the turbulence created in the bed. The material to be dried and hot air are in cross-flow with respect to the direction of flow of each other. The residence time can be controlled from seconds to hour. The moist air from the drier containing fines is admitted to a cyclone separator for the recovery of fines.</p>	
2-c	<p>Reflux ratio is the ratio of amount of distillate fed back to the column to the amount of liquid taken out as distillate or top product.</p> <p>It is represented by 'R'</p> $R = L/D$ <p>Reflux improves purity: By allowing reflux, liquid and vapour phases are coming into contact with each other on every plate and mass transfer takes place every time. This will make the vapour richer in more volatile component and liquid in less volatile component. Thus the composition of more volatile component in the final distillate will be more, hence the purity.</p>	<p>2</p> <p>2</p>
2-d	<p>Expression for operating line of rectifying section:</p>	



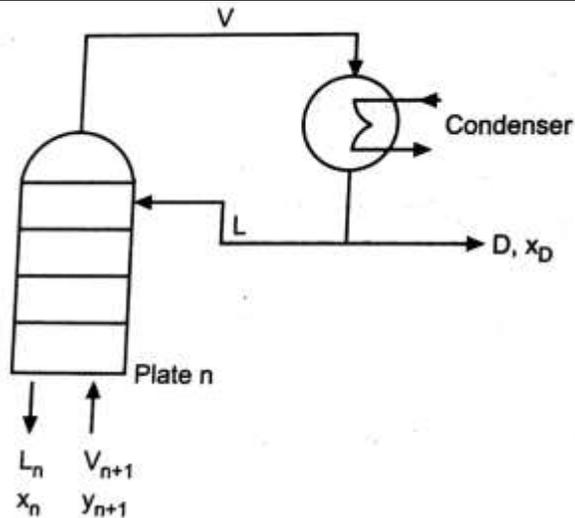
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Material balance around condenser is

$$V = L + D$$

$$\text{Or } L = V - D ; D = V - L$$

Overall balance is

$$V_{n+1} = L_n + D$$

Component balance for A

$$V_{n+1} y_{n+1} = L_n x_n + D x_D$$

$$y_{n+1} = L_n x_n / V_{n+1} + D x_D / V_{n+1}$$

$$\text{But } V_{n+1} = L_n + D$$

$$y_{n+1} = L_n x_n / L_n + D + D x_D / L_n + D$$

This is Expression for operating line of rectifying section.

1

1

1

1

2-e

Triangular diagram:



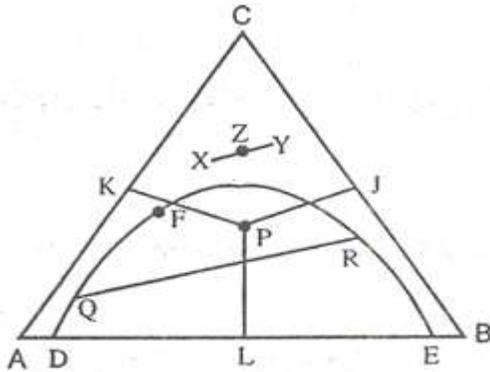
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2

Where

A=diluent

B=solvent

C=solute

Uses: In liquid-liquid extraction, when the solvent is partially miscible with the original solvent, the solubility and equilibrium relations are often shown on a triangular diagram. The composition of ternary system can be shown by a point lying inside an equilateral triangle

2

This is used to find equilibrium between extract phase and raffinate phase.

It is used to give concept of tie line, plait point

It can be used for finding out number of stages for complete recovery of solute.

Binodal curve: It represents two phase region that will split up into two layers in equilibrium with each other.

Tie line: Tie line is a line which connects two phases in equilibrium with each other.

Plait point: The plait point on binodal solubility curve represent a single phase where the length of tie line is zero.



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3	Attempt any 2	16
3-a	<p>q-line: The 'q' is a measure of the thermal condition of the feed and is defined as the number of moles of saturated liquid resulting in the stripping section for each mole of feed introduced. Thus for a feed we get ,</p> $L' = L + qf$ $V = V' + (1-q)F$ <p>Derivation of q-line :</p> <p>The liquid flow in the stripping section is</p> $L' = L + qf$ $\therefore L' - L = qf \quad \text{----- (1)}$ <p>Similarly, the vapour flow in the rectifying section is</p> $V = V' + (1 - q) F \quad \text{----- (2)}$ $\therefore V - V' = (1 - q) F \quad \text{----- (3)}$ <p>Overall material balance in the upper section of coloumn :</p> $V = L + D \quad \text{----- (4)}$ <p>Material balance of A in the upper section :</p> $V_y = Lx + D x_D \quad \text{----- (5)}$ <p>Overall material balance in the lower section :</p> $V' = L' - W \quad \text{----- (6)}$ <p>Material balance of A in the lower section :</p> $V'y = L'x - W x_w \quad \text{----- (7)}$ <p>Subtracting Equation (7) from Equation (5)</p> $y (V - V') = x (L - L') + D x_D + W x_w \quad \text{----- (8)}$ <p>Overall material balance of A over the coloum as a whole :</p>	4



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$$x_f \cdot F = D x_D + W x_w \quad \text{----- (9)}$$

∴ Equation (8) becomes

$$y (V - V') = x (L - L') + x_F \cdot F \quad \text{----- (10)}$$

Substituting the values of $V - V'$ and $L' - L$ from Equation (3) and (1) into Equation (10) gives

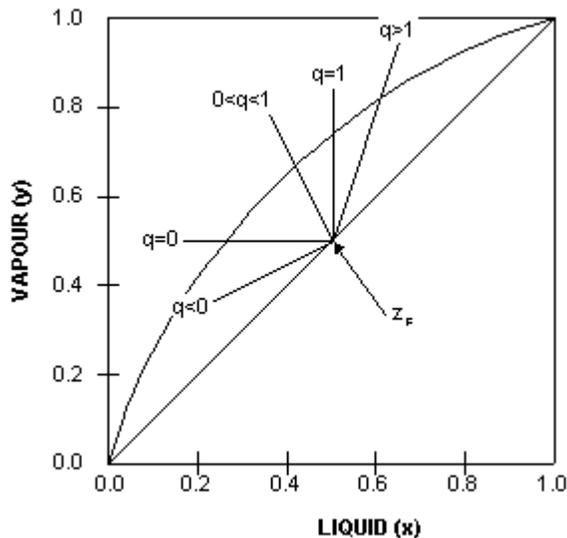
$$y (1 - q) F = x(-qF) + x_F \cdot F$$

$$\therefore y = \frac{-q}{1-q} x + \frac{x_F}{(1-q)} \quad \text{----- (11)}$$

Equation (11) is known as the **feed line or q-line** equation

Types of q lines for various feed conditions:

- q = 0 (saturated vapour)
- q = 1 (saturated liquid)
- 0 < q < 1 (mix of liquid and vapour)
- q > 1 (subcooled liquid)
- q < 0 (superheated vapour)





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	<p>Operating line of rectification section: Point A(0.966,0.966) on the diagonal. The intercept of the rectifying section of operating line is = $x_D / R + 1$ $= 0.966 / 3.14 + 1 = 0.232$ From the graph the theoretical stages required including reboiler = $n = 10$. Number of stages required in column = $n - 1 = 10 - 1 = 9$</p>	<p>1 1</p>
<p>3-c</p>	<p>Lewis Sorel method of determination of number of theoretical plates: Equation of operating line of rectifying</p> $y_{n+1} = \frac{L_n}{L_n + D} x_n + \frac{D \cdot X_D}{L_n + D} \quad \text{eq.1}$ <p>Operating line of stripping section</p> $y_{m+1} = \frac{L_m}{L_m - W} x_m - \frac{W \cdot X_W}{L_m - W} \quad \text{eq.2}$ <ol style="list-style-type: none"> 1. From the data cited in a given problem, evaluate the terms – D,W,L,etc. 2. From the x-y data provided (or can be generated knowing the relative volatility) draw an equilibrium diagram. 3. Substitute the values of $L_n(L)$, x_D, D in equation(1), in order to get a relationship between y_{n+1} and x_n. 4. Similarly, substitute the values L_m, W, x_W in equation(2), to get a relationship between y_{m+1} and x_m. L_m is to be evaluated by taking into consideration the condition of feed. For example, if it is a liquid at its bubble point $L_m = L_n + F$. 5. The distillate composition (x_D) given in the problem statement represents 	<p>8</p>



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	<p>the composition of vapour (y_n) as it is obtained by condensing the vapour leaving the column.</p> <p>6. From the vapour phase composition : $y_n = x_D$, find the liquid phase composition x_{n+1} from the x-y curve drawn and substitute the value of x_{n+1} in the equation of the operating line of the rectifying section to get y_2</p> <p>7. Find x_{n+2} value from the equilibrium diagram corresponding to y_{n+2}</p> <p>8. Find y_{n+3} and proceed with the same equation till we reach the point when the liquid phase composition equal to or less than x_F</p> <p>9. Then make use of the material balance equation or operating line of stripping section and proceed in the same way as described above till we get the liquid phase composition equal to or below x_W, suppose we end with y_{n+10}, it means that there will be 10 plates in the column.</p>																
4 A	Attempt any 3	12															
4A-a	<p>Differentiate between distillation and extraction</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 30%;">points</th> <th style="width: 35%;">Distillation</th> <th style="width: 35%;">Extraction</th> </tr> </thead> <tbody> <tr> <td>Thermal energy</td> <td>Requires thermal energy</td> <td>Requires mechanical energy for mixing and separation</td> </tr> <tr> <td>Operating cost</td> <td>Cost is Low.</td> <td>Cost is high.</td> </tr> <tr> <td>Equipment</td> <td>Needs heating and cooling provisions</td> <td>Doesn't need heating and cooling provisions</td> </tr> <tr> <td>Quality of product</td> <td>Gives almost pure product</td> <td>Doesn't give pure product</td> </tr> </tbody> </table>	points	Distillation	Extraction	Thermal energy	Requires thermal energy	Requires mechanical energy for mixing and separation	Operating cost	Cost is Low.	Cost is high.	Equipment	Needs heating and cooling provisions	Doesn't need heating and cooling provisions	Quality of product	Gives almost pure product	Doesn't give pure product	1 mark each
points	Distillation	Extraction															
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4A-b	<p>Equation for steady state equimolar counter diffusion for gases:</p> $N_A = D_{AB} / RTZ (P_{A1} - P_{A2})$	2															



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	<p>Where N_A = molar flux of A D_{AB} = Diffusivity of A in B R = Universal gas constant T = absolute temperature Z = distance through which diffusion occurs P_{A1} = partial pressure of A at beginning of diffusion P_{A2} = partial pressure of A at end of diffusion</p>	2
4A-c	<p>Application of Steam Distillation:</p> <ol style="list-style-type: none">1. For separating high boiling component from non volatile impurities.2. For separating high boiling mixture into different fractions wherein the decomposition of material might occur if direct distillation were employed3. Where vaporization temperature cannot be reached by heat <p>Application of batch Distillation:</p> <ol style="list-style-type: none">1. Where small quantities of liquid mixture are to be handled.2. When more than one product is to be obtained3. When liquid mixture to be separated are high in solid content. <p>Steam distillation:</p> <p>Steam distillation is adopted in cases where substance involved cannot withstand temp of distillation and decompose. Substance of this kind can be separated by reducing the partial pressure of the volatile component. This can be done by making use of inert vapour that decreases the temperature of distillation. The inert vapour used should be practically immiscible with components to be distilled. Steam is used for this purpose.</p> <p>In steam distillation, steam is directly admitted into the liquid in the still. The mixed vapour containing desired component is taken as overhead, condensed and desired component is separated from water phase by gravity while non volatile material remains behind in the still.</p>	<p>½ mark each for any 2</p> <p>½ mark each for any 2</p> <p>2</p>



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4A-d	<p>Most common packings are :</p> <ol style="list-style-type: none">1) Raschig rings.2) Pall rings.3) Hy-pak.4) Berl saddles.5) Intalox saddles.6) Super intalox saddles7) Lessing ring <p>Characteristics of a tower packing :</p> <ol style="list-style-type: none">1) It should provide a large interfacial area for phase contacting2) It should possess good wetting characteristics.3) It should have a high corrosive resistance.4) It should be relatively cheap.5) It should possess enough structural strength.6) It should be chemically inert to the fluids handled in the tower.	<p>½ mark each for any 4</p> <p>½ mark each for any 4</p>
4B	Attempt any 1	6
4B-a	Mixer settler:	



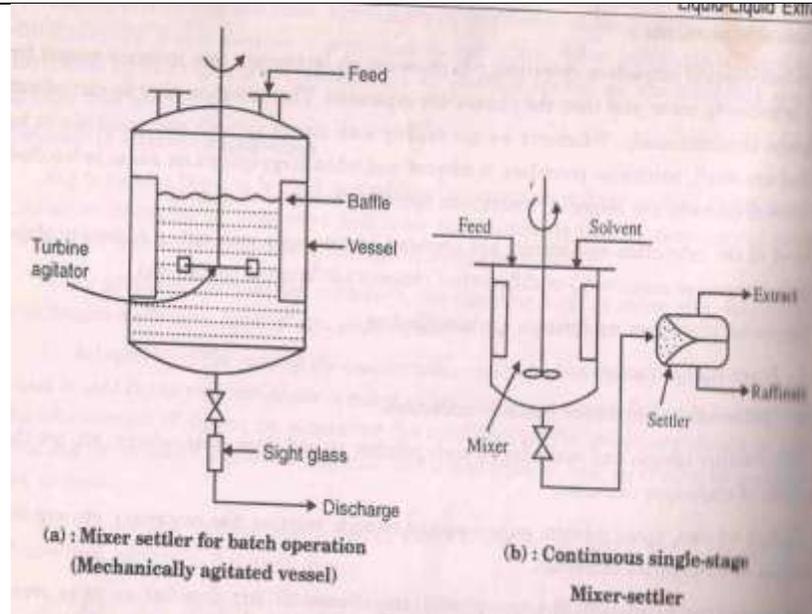
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3

The mixer-settler is the most simple type of extractor. It is a stage-type extractor and has many variations.

Construction and working: For extraction operations carried out batch wise, the mixture and settler may be the same unit (fig.a). It consists of a vertical tank incorporating a turbine or propeller agitator. It is provided with charging nozzles at the top and discharge connection carrying a sight glass at the bottom. Feed solution to be extracted is taken into an agitated vessel, and then the required amount of solvent is added, and whole mass is agitated for predetermined time. At the end of mixing cycle, agitation is stopped and settling is applied for a phase separation. Afterwards, the raffinate and extract phases are withdrawn from the bottom into separate receivers.

For continuous operation, the mixer and settler are separate units Fig.(b). The mixer is a small baffled agitated tank provided with inlet-outlet connections and settler is often a continuous gravity decanter. In this extractor, two phases are

3



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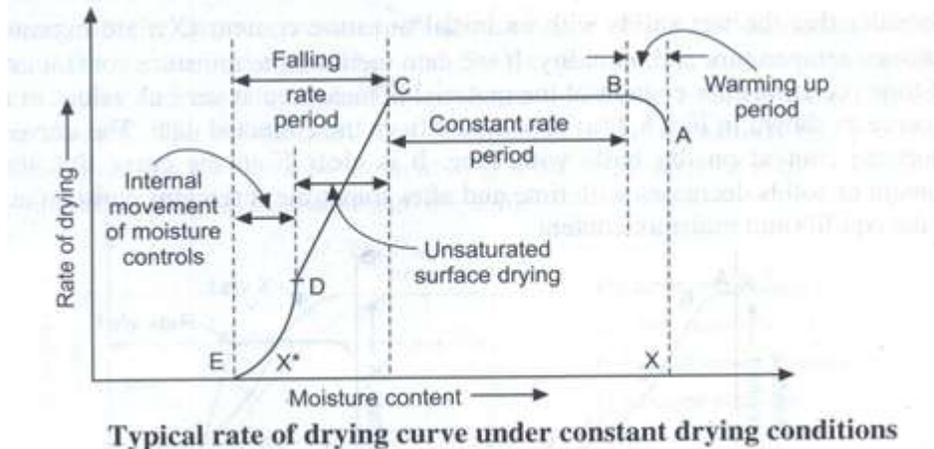
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continuously in contact with each other in the mixer under thorough agitation before flowing to settler for phase separation.

4.B b

Rate of drying curve :



2

Rate of drying curve is plotted with rate of drying on y-axis and moist. Content on x-axis.

Section AB of the curve represents the **warming up period** during which this temperature of the solid is becoming equal to the temperature of drying air. BC is straight line that to x-axis in presenting **constant rate** of drying during which the layers of water on the surface of solid is being evaporated. The section CE of the curve represents the **falling rate period** composing of first falling rate period CD and second falling rate period DE from point C onwards some dry patches have started forming on the surface of the solid. The rate of drying decreases for the unsaturated portion and hence rate for total surface portion and hence rate for total surface decreases. The section CD of the curve represents the period corresponding to the zone of unsaturated surface drying the moisture content at which constant rate period ends is known as critical moisture content. After point D, the surface of the solid is completely dry and

4



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	Methanol balance is $0.35 \times 100 = 0.965X + 0.1Y$(2) Solving (1) and (2) $X = 28.9$ kmoles and $Y = 71.1$ kmoles Molal flow rate of distillate = 28.9 kmoles/h Molal flow rate of bottom product = 71.1 kmoles/h	1 1
5-e	Relative merits of plate and packed columns <ol style="list-style-type: none">1. Plate columns operate over a wide range of liquid flow rates without flooding.2. Plate columns by repeated mixing and separation provide more positive contact between fluid phases.3. Because of difficulties arising in dispersion of liquid in packed tower, plate tower is more reliable.4. Side streams are very easily taken out from plate towers5. For plate towers, design information is generally more readily available.6. Whenever liquid mixtures containing dispersed solids are to be handled, plate towers should be preferred.7. Whenever inter stage cooling is required, plate towers are preferred.8. For a given duty, total weight of dry plate tower is less than the weight of packed towers.9. High values of liquid- gas ratio are best handled in packed tower.10. For liquids having tendency to foam, packed towers are preferred.11. The liquid hold up is low in packed tower.12. Pressure drop through packed tower is usually low.13. Packed towers are more economical when highly corrosive fluids are to be handled.14. Plate towers are preferred when large temperature changes are involved.	½ mark each for any 8
6	Attempt any 2	16
6-a	Initial moisture content $X_1 = 0.67 / (1 - 0.67) = 2.03$	1



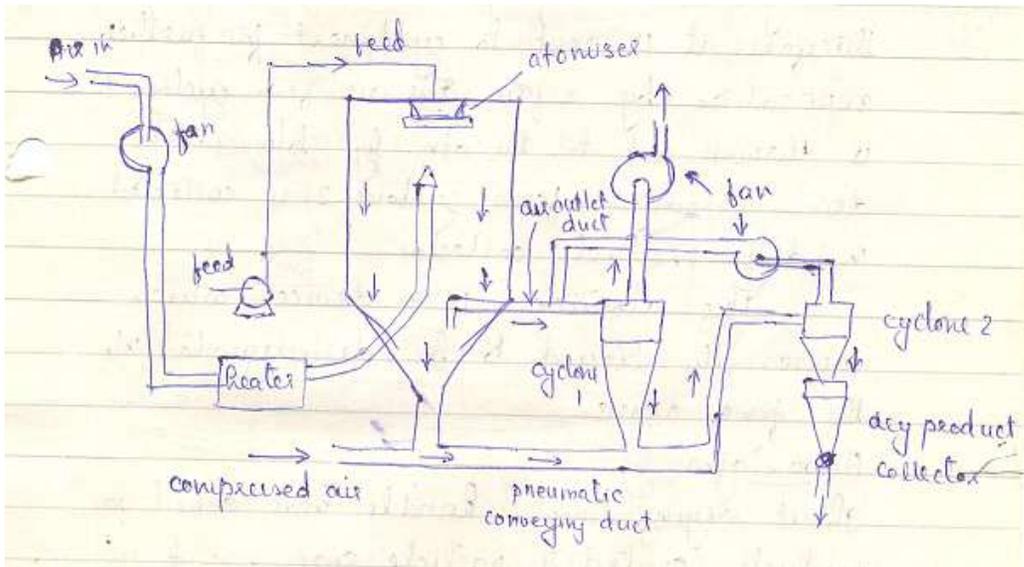
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	<p>Final moisture content $X_2=0.25/(1-0.25)=0.333$</p> <p>Equilibrium moisture content $X^*=0.01/(1-0.01)=0.0101$</p> <p>Critical moisture content $X_c=0.4/(1-0.4)=0.67$</p> <p>$R_c = 1.5 \text{ kg/ m}^2 \text{ hr.}$</p> <p>$A/W'=0.5 \text{ or } W'/A=2$</p> <p>$t = W'/AR_c \{ (X_1-X_c) + (X_c - X^*)\ln[(X_c - X^*)/(X_2 - X^*)] \}$</p> <p>$= 2/1.5 \{ (2.03-0.67) + (0.67 - 0.0101)\ln[(0.67 - 0.0101)/(0.333 - 0.0101)] \}$</p> <p>= 2.44 hr.</p>	<p>1</p> <p>1</p> <p>1</p> <p>1</p> <p>1</p> <p>2</p>
<p>6-b</p>	<p>Spray Dyer :</p>  <p>It is continuous direct contact dryer employed for drying of solutions, slurries and pastes. In this dryer, the feed is introduced in the form of very fine droplets into a stream of hot gas.</p> <p>Construction: It consists of a drying chamber where feed is contacted with hot gas, heater for heating fresh air sucked by fan or blower, cyclone separators for dust separation and collection, pneumatic conveying duct and blowers. The</p>	<p>3</p> <p>2</p>



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	<p>material is spread in the form of a mist of fine droplets by spray nozzles, into a hot gas stream inside the chamber.</p> <p>Working :</p> <p>The feed is pumped to the top of this dryer where it is disintegrated into small droplets by atomizers. The large quantity of fresh air is taken in by fan, it is heated in the heater and finally fed below the atomizer in drying chamber. As the surface area of drops is very large, the liquid portion of these drops rapidly evaporates and before they touch the bottom of drying chamber they are completely dried. The dried product is taken out and conveyed in the cyclones dust collector by stream of air major portion of the air is taken out through air outlet duct which mostly contains dust and is sent to cyclones. The solids collected are fed to pneumatic conveying duct. The air leaving the cyclone may contain some dust and therefore it is sent to cyclone 1 for further separation by a fan., The air from cyclone 1 is thrown out to the atmosphere by blower. The dried product from cyclone 2 is connected in dry product connector.</p>	3
6-c	<p>Basis 1000 kg feed solution at 353K</p> <p>$F=1000 \text{ kg. } x_F=64.2/164.2= 0.391$</p> <p>Water in feed = $1000(1-0.391) = 609 \text{ kg}$</p> <p>Water evaporated = $0.1*609= 60.9 \text{ kg}$</p> <p>Mol wt of $\text{MgSO}_4=120$, Mol wt of $\text{MgSO}_4 \cdot 7\text{H}_2\text{O} = 246$</p> <p>Solvent balance is</p> <p>$F(1- x_F) = V+C(126/246)+ L$</p> <p>$100 (1-0.391)=60.9+0.5122C+L$</p> <p>or $L=609-60.9+0.5122C \text{ kg.}$</p> <p>$\text{MgSO}_4$ balance</p> <p>MgSO_4 in feed = MgSO_4 crystals + MgSO_4 in mother liquor.</p>	1 1 1 1 1 1



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	0.391*1000=C(120/246)+[609-60.9+0.5122C] * solubility of NaNO ₃ 391 = 0.488C+[609-60.9+0.5122C]*0.408 Or C=599.7 kg Yield of MgSO ₄ crystals (C)= 599.7 kg.	1 1
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